

Scaling of edge turbulence properties and implications for the SOL width

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NSTX-U

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Background – theory

- Theory-based scaling of the SOL heat flux width by turbulence
 - J. W. Connor, et al., Nucl. Fusion **39**, 169 (1999)
 - F. D. Halpern, et al., Nucl. Fusion **53**, 122001 (2013)
 - J. R. Myra et al., Phys. Plasmas **22**, 042516 (2015)

$$\frac{q_{\perp}}{\lambda_q} = \frac{q_{\parallel}}{L_{\parallel}} \sim \frac{g p c_s}{qR}$$

$q_{\parallel} \equiv g p c_s$
 $g = \text{parallel energy transmission factor}$

$$\lambda_q \approx \frac{qR}{g} \frac{q_{\perp}}{p c_s} = \frac{qR}{g} \frac{\langle \delta v_x \delta p \rangle}{c_s p}$$

- Obtain scalings for $\lambda_q(R, \rho_s, q, \dots)$ once we know turbulence properties
 - $\delta v_x/c_s, \delta p/p$ which depend on:

- type of instability
- wavenumber or scale size $k\rho_s, k\lambda_p$
- saturation mechanism
- type of transport

drift-resistive?
 curvature? flow?
 quasi-local? nonlocal?
 wave-breaking?
 profile modification?
 sheared flows?

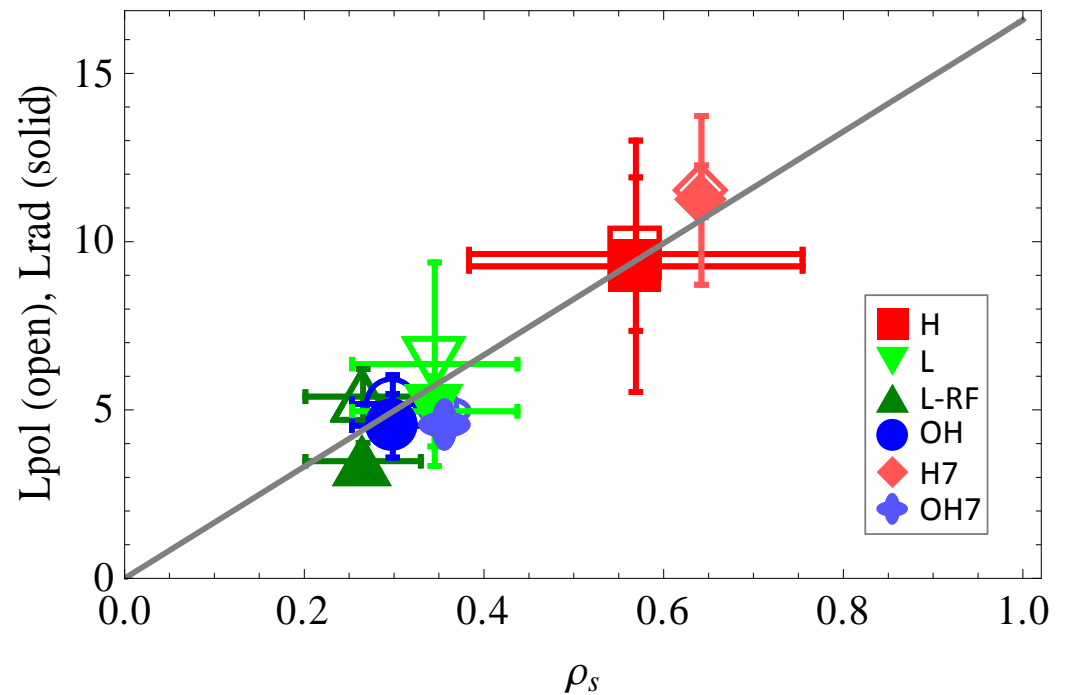
- PoP 2015 analysis $\Rightarrow \lambda_q \propto R^{\mu}$ with $1/3 < \mu < 1$
- Challenge and expand this approach with experimental data & computation

Background – NSTX edge turbulence database

- Comprehensive edge database for NSTX using gas puff imaging (GPI)
 - S. J. Zweben, et al., *Nucl Fusion* **55**, 093035 (2015)
 - 140 NSTX discharges,
 - 93 H mode
 - 9 (neutral beam heated) L mode
 - 5 (high harmonic fast wave heated) L-RF mode
 - 33 OH mode
- High quality subset “blob” database
 - S. J. Zweben, *Plasma Phys. Control. Fusion* **58**, 044007 (2016)
 - 7 similar H modes and 7 similar OH modes
- This talk: databases examined and interpreted based on theoretical estimates relevant to SOL width scaling
 - complementary to pure theory-based work
 - obtain information on near-separatrix turbulence:
 - time and spatial scales; saturation levels, type of instability
 - inferences for scaling

Length scale of edge turbulence consistent with drift waves

- Turbulence scale lengths from GPI correlation analysis in the edge (Zweben 2015)
- $L_{\text{pol}} \sim L_{\text{rad}} \sim 17 \rho_s \Rightarrow k_{\perp} \rho_s \sim 0.13$
- Consistent with drift waves or drift-resistive modes
- Note scaling between different operational modes
- Data at -2 cm (just inside separatrix) here and in following
- Error bars \Rightarrow std. dev. (not uncertainty of the means)

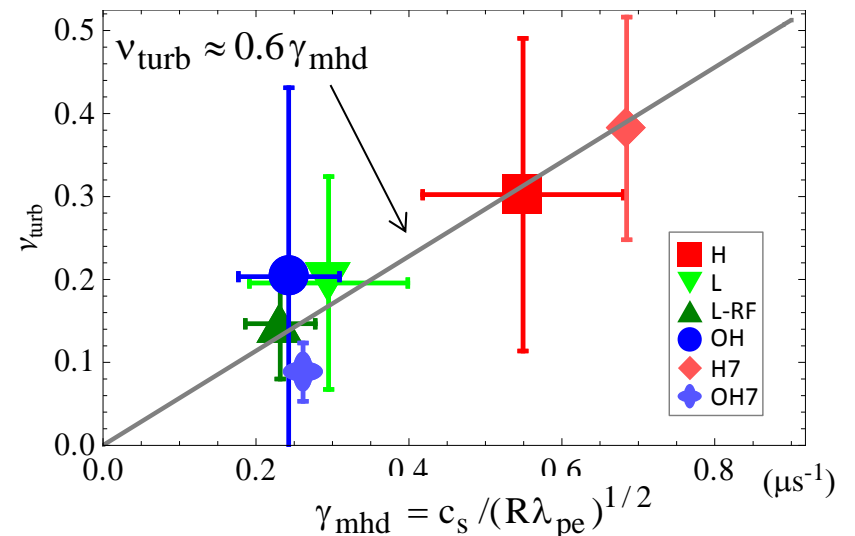
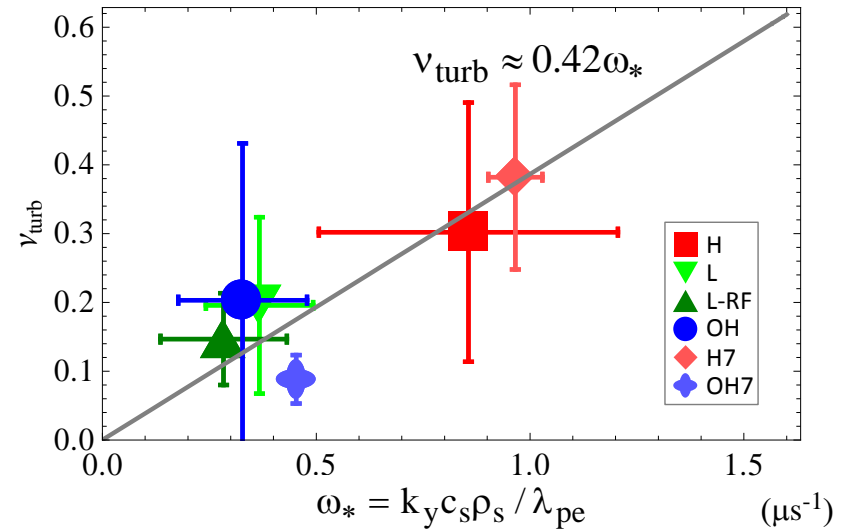


Time scale of turbulence consistent with drift-interchange

- Auto-correlation time dominated by convection (of moving structures and spatial size). Need a measure of time scale in the local plasma frame.
- Define v_{turb} from continuity equation assuming $E \times B$ convection

$$v_{\text{turb}} \delta p = \delta v_x p / \lambda_p$$

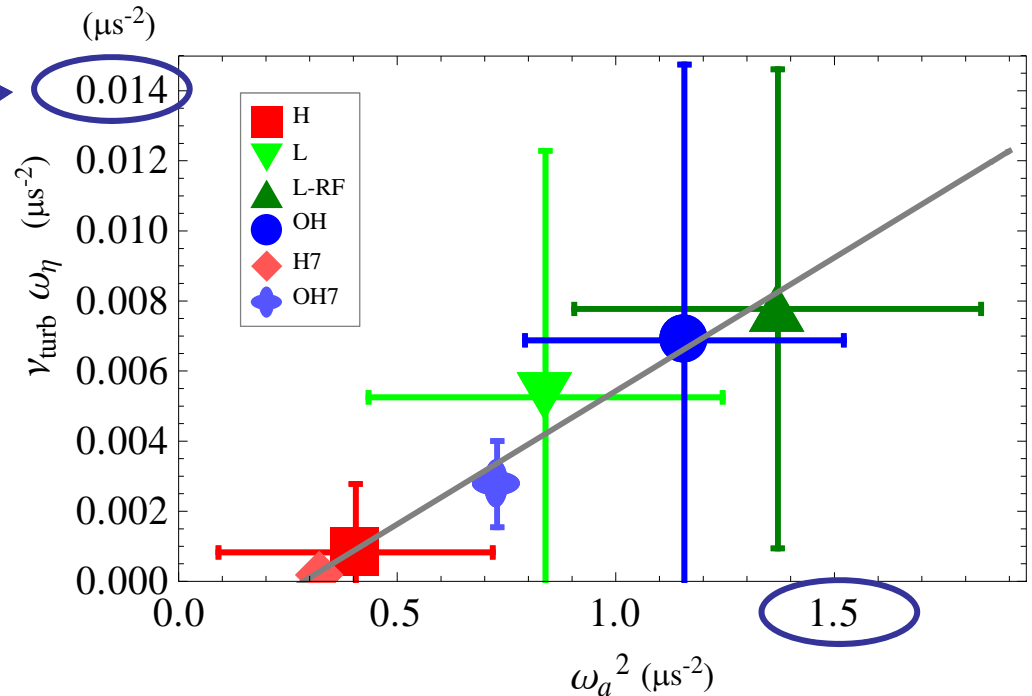
- Use v_{turb} as a proxy for ω in the plasma frame
- Estimate $\delta p/p \sim \delta I/I$ (GPI intensity)
- Scaling is consistent with both drift waves and curvature-driven interchange



X-pt enhanced resistive ballooning is likely in OH & L modes

- In the resistive ballooning equation, resistivity overcomes EM line bending when $\omega\omega_\eta > \omega_a^2$
 - where the magnetic diffusion rate is given by $\omega_\eta = k_\perp^2 \delta_e^2 v_{ei}$, $\delta_e = c / \omega_{pe}$
 - the Alfvén frequency is $\omega_a = v_a / R$

- Resistivity is weak at the outer midplane
 - need k_\perp enhanced by ~ 14 ✓
 - resistive X-point physics likely in OH and L modes:
 - Xu PoP 2000
 - Myra PoP 2000



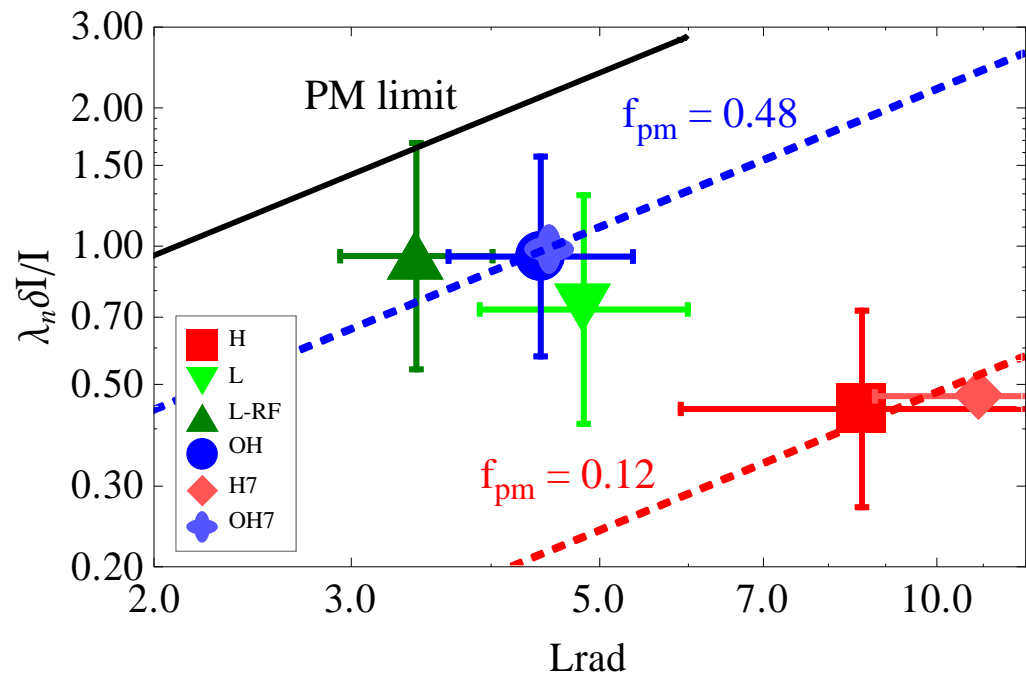
Saturation level is near (OH, L) or well below (H) PM limit

- Profile modification (PM) limit: $\frac{\delta n}{n} = \frac{f_{pm}}{k_x \lambda_n}$

$f_{pm} = \text{scaling factor}$

 - compares fluctuation and equilibrium gradients

- Estimate $k_x \sim 2.1/L_{rad}$
- OH and L modes near PM limit (less so if $\lambda_n \rightarrow \lambda_p$)
- H mode far below
 - sheared flow turbulence suppression?



See also (Zweben NF 2015)

Scaling implications for the SOL width

- Eliminating δv_x using v_{turb} and expressing in terms of f_{pm}

$$\lambda_q = \frac{qR}{g} \frac{\langle \delta v_x \delta p \rangle}{c_s p} \rightarrow \lambda_q \approx \frac{qR}{g} \frac{f_{\text{pm}}^2 v_{\text{turb}}}{k_x^2 \lambda_p c_s}$$

- Invoking the drift-interchange character

$$v_{\text{turb}} = C_{\text{dw}} \omega_* = \frac{C_{\text{dw}} k_y c_s \rho_s}{\lambda_p} \quad \text{and} \quad v_{\text{turb}} = C_{\text{mhd}} \gamma_{\text{mhd}} = \frac{C_{\text{mhd}} c_s}{(R \lambda_p)^{1/2}}$$

- Equating the two expressions $\frac{\lambda_p}{R} = \frac{C_{\text{dw}}^2 C_{\text{k}\rho}^2}{C_{\text{mhd}}^2}$ where $C_{\text{k}\rho} \equiv k_y \rho_s$

- For H-modes there is another plausible constraint:

- expect the $\mathbf{E} \times \mathbf{B}$ shearing rate induced by ion diamagnetic drifts to compete with the interchange drive

$$\gamma_{\text{mhd}} \leq V'_{\text{di}} \Rightarrow \frac{c_s}{(R \lambda_p)^{1/2}} \leq \frac{c_s \rho_s}{\lambda_p^2} \Rightarrow \lambda_p \leq R^{1/3} \rho_s^{2/3}$$

Scaling implications for H-modes

- Define C_λ by $\lambda_p = C_\lambda R^{1/3} \rho_s^{2/3}$
 - for NSTX H-modes $C_\lambda \sim 0.3$
- Combining with previous results

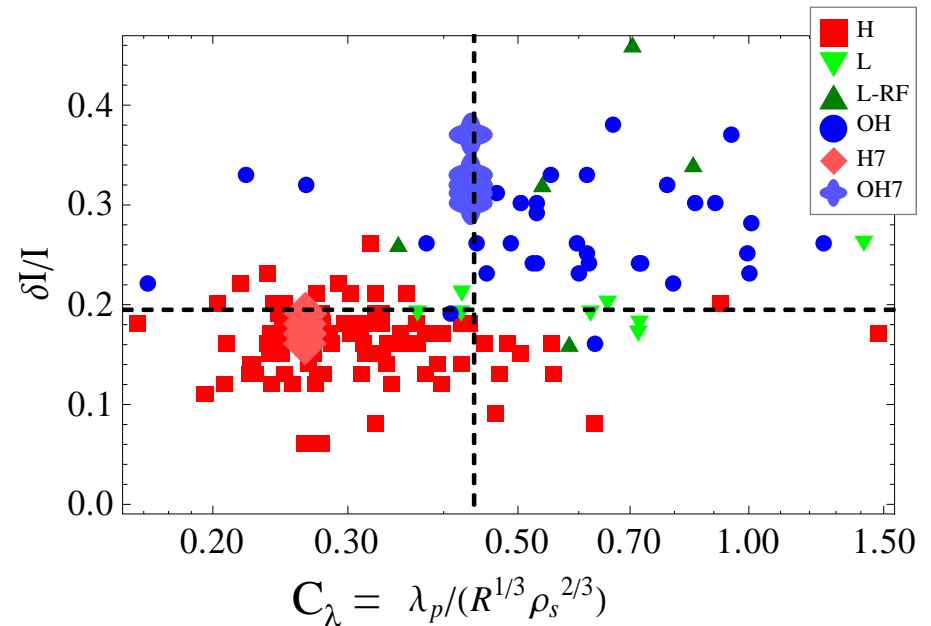
$$\frac{\lambda_p}{R} = \frac{C_{dw}^2 C_{kp}^2}{C_{mhd}^2}, \quad \frac{\rho_s}{R} = \frac{C_{dw}^3 C_{kp}^3}{C_{mhd}^3 C_\lambda^{3/2}}$$

drift-interchange sheared flow

- and finally

$$\lambda_q = \frac{qR}{g} \left(\frac{f_{pm}^2 C_{dw}^3 C_{kp}}{C_{mhd}^2 C_\lambda^3} \right) \approx \frac{qR}{g} \left(\frac{f_{pm}^2}{51 C_\lambda^3} \right)$$

normalized perp heat flux: expressed entirely in terms of 5 measured dimensionless quantities



- \Rightarrow
- 0.2 to 0.8 cm using previous $C_{mhd}, C_{dw} \dots$
 - comparable to IR measurements
 - explicit $\lambda_q \propto qR \propto \varepsilon^2 RB / I_p$
 - difficult to separate out mechanisms

Numerical simulation

- The five dimensionless ratios that determine the turbulent perpendicular heat flux in the preceding analysis are:

$$C_{dw} = v_{\text{turb}} / \omega_*$$

$$C_{\text{mhd}} = v_{\text{turb}} / \gamma_{\text{mhd}}$$

$$C_{k\rho} = k_y \rho_s$$

$$C_\lambda = \lambda_p R^{-1/3} \rho_s^{-2/3}$$

$$f_{\text{pm}} = (k_x \lambda_n) (\delta n / n)$$

} drift interchange

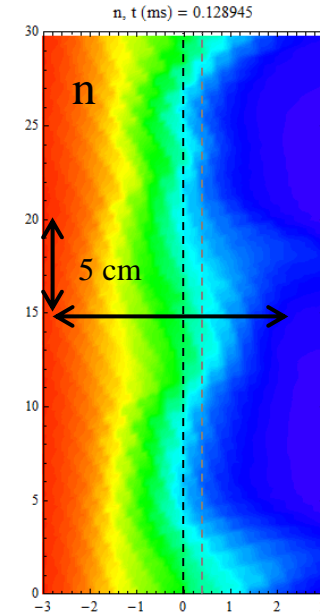
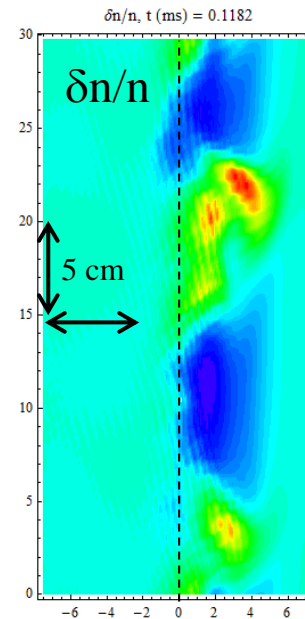
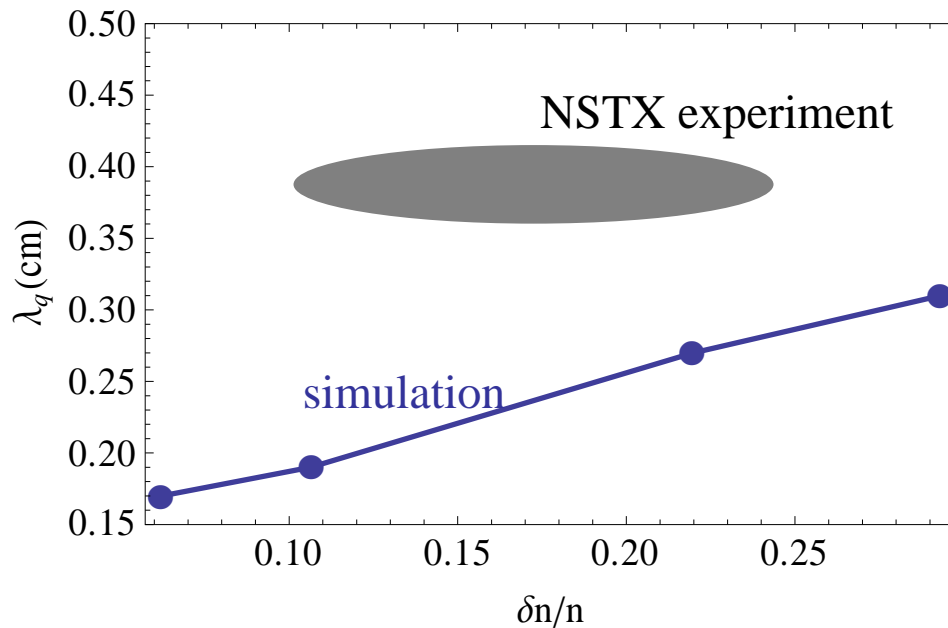
sheared flow H-mode

saturation level

- Measured inside the separatrix (turbulence generation) but drive transport into the SOL
- Assess role of drift-interchange physics, sheared flows and resulting saturation levels.
 - compare with experiment; test theoretical scalings
- SOLT code (reduced 2D fluid turbulence model for edge/SOL)
- XGC1 5D kinetic simulations [S. Ku, R.M. Churchill, C.S. Chang, J.R. Myra, S.E. Parker]

SOLT code simulation

- Simulate NSTX H-mode #127975 ($I_p = 1\text{ MA}$, $P_{\text{NBI}} = 6\text{ MW}$, $B_t = 0.4\text{ T}$)
 - prepared for 2016 theory milestone: thanks to Maingi, Ahn, Gray, Canal
- Interpretive SOLT simulations: varied sources, R_{sep} , diffusion to match
 - measured n_e , T_e profiles, P_{sol} , $(\delta n/n)_{\text{sep}}$
- Vary turbulent dissipation $\Rightarrow (\delta n/n)_{\text{sep}}$ to test effect on λ_q



- Turbulence is neither dominant or negligible at $I_p = 1\text{ MA}$
 - leaves room for NC drift to explain dominant $1/I_p$ scaling
 - leaves room for turbulence at larger I_p or larger R

Conclusions

- Scalings of edge turbulence in NSTX emerge among operational modes
 - $k_y \rho_s \sim 0.13$; $\omega \sim 0.4 \omega_* \sim 0.6 \gamma_{\text{mhd}}$
 - consistent with drift-interchange modes
- 5 dimensionless numbers characterize the turbulent perpendicular heat flux for drift-interchange modes
 - evaluated from the NSTX database and theoretical considerations
- Quantitative estimates and simulations for the turbulent contribution to λ_q suggest that it is not negligible, at least for discharges with high plasma current.
 - λ_q based on this physics has an explicit positive scaling with R