Diagnosing ablator $\rho R$ and $\rho R$ modulations in capsule implosions using charged-particle spectrometry at the National Ignition Facility

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By fielding several compact proton spectrometers at various locations around an ignition-capsule implosion at the National Ignition Facility [G. H. Miller, E. I. Moses, and C. R. Wuest, Nucl. Fusion 44, S228 (2004)], $\rho R$ and $\rho R$ modulations of the ablator for a failed implosion can be obtained through absolute measurements of knock-on proton (KO-P) spectra. For ignition capsules with a Cu-doped beryllium (Be) ablator, 50:50 mixture of deuterium-tritium (DT) fuel and $\sim 1\%$ residual hydrogen (H) by atom, failed implosions can be diagnosed for neutron yields ranging from $\sim 10^{11}$ to $\sim 6 \times 10^{15}$ and local $\rho R$ up to $\sim 240 \text{ mg/cm}^2$. For capsules with an ablator of Ge-doped CH, which contains a large amounts of H, failed implosions can be diagnosed for neutron yields ranging from $\sim 10^{10}$ to $\sim 6 \times 10^{15}$ and local $\rho R$ up to $\sim 200 \text{ mg/cm}^2$. Prior to the first ignition experiments, capsules with a Cu-doped Be ablator (or Ge-doped CH ablator), more deuterium-lean fuel mixture and H-dopant levels up to $25\%$ in the fuel will be imploded to primarily reduce the neutron yield. The HDT-filled Be-capsule implosion, which can be diagnosed for neutron yields ranging from $\sim 5 \times 10^8$ to $\sim 6 \times 10^{15}$ and local $\rho R$ up to $\sim 240 \text{ mg/cm}^2$, is more suitable to diagnose using KO-Ps as the signal-to-background ratio is significantly higher than for an ignition-capsule implosion. In addition, analysis of CH-ablator data obtained from analogous OMEGA [T. R. Boehly, D. L. Brown, R. S. Craxton et al., Opt. Commun. 133, 495 (1997)] experiments indicate that the shape of the KO-P spectrum is affected mainly by the ablator $\rho R$. Other effects such as ablator-density-profile variations, time evolution of the ablator $\rho R$, fuel-ablator mix and electron temperature variations typically predicted for the ablator play minor roles. © 2008 American Institute of Physics. DOI: 10.1063/1.2965829

I. INTRODUCTION

Ignition of an indirectly laser-driven capsule implosion at the National Ignition Facility (NIF) (Ref. 1) requires careful tuning of the drive conditions to the capsule parameters.2–5 Inadequate knowledge about the drive physics is therefore a serious concern, since an underdriven or over-driven capsule will leave too much or too little ablator mass as payload and thus reduce the performance of an implosion to the point it fails to ignite.2 If the initial ablator is too thin, it burns through too quickly and the implosion fails to ignite due to preheat or instability issues; or if the initial ablator is too thick, the implosion velocity is too low and the implosion fails to ignite due to poor compression. To address this issue, we propose to accurately diagnose the areal density ($\rho R$) of the ablator using charged-particle spectrometry. By fielding several compact charged-particle spectrometers (spectrometer housing is less than 5 cm in diameter) at various locations around a NIF implosion, $\rho R$ and $\rho R$ modulations of the ablator can be obtained through measurements of spectra of knock-on protons (KO-P) elastically scattered by primary DT neutrons.7 The KO-Ps have a well known, flat birth spectrum ranging from 0 to 14 MeV, and as they traverse through the ablator they lose energy in proportion to the amount of material they pass through ($\rho R$). A $\rho R$ value for the portion of the implosion facing a given spectrometer can therefore be determined from the energy downshift and shape of the measured KO-P spectrum by applying a newly developed analysis technique, which utilizes Monte Carlo modeling of an implosion and the plasma-stopping power formalism described in Ref. 9. Using this technique, it is shown in this work that the shape of the spectrum of the escaping KO-P can be used to accurately diagnose a variety of ablator compositions for neutron yields up to $\sim 6 \times 10^{15}$ and ablator $\rho R$ up to $\sim 240 \text{ mg/cm}^2$. The work described herein improves and extends significantly the work by Nakaishi et al.,10 Li et al.,11 and Frenje et al.,12 who used a relatively simple implosion model to relate the $\rho R$ to the measured KO-P yield. Nakaishi et al. applied the yield method to a coarse KO-P spectrum measured in a single direction for a thin-glass microballoon capsule implosion; while Li et al. and Frenje et al. used the yield method to infer a fuel $\rho R$ from high-resolution KO-P spectra obtained simultaneously in several different directions for ICF relevant capsule implosions. However, as noted by Frenje et al.,12
This yield method is subject to significant spatial-yield variations caused by magnetic fields surrounding an implosion prohibiting $pR$ modulations to be diagnosed. As a result, only an average $pR$ can be obtained from several spectrometers fielded around an implosion using this method. In this context, it is important to note that Seguin et al.\textsuperscript{13} and Hicks et al.\textsuperscript{14} demonstrated that the energies of the KO-Ps are not affected when bang time occurs after the laser pulse (when the electrical field has decayed away). This is also the case for the NIF-capsule implosions discussed in this work. According to simulations, the bang time occurs typically a nanosecond after the laser pulse has been turned off for these implosions. Measurement of the KO-P spectrum is therefore a much more powerful method than the yield method for diagnosing the ablator $pR$ of an implosion at the NIF, and in general.

In addition, the KO-P measurements and analysis techniques described herein will nicely complement and extend the work by Wilson et al.,\textsuperscript{15} Hicks et al.,\textsuperscript{16} and Olson et al.\textsuperscript{17,18} that were carried out mainly at the OMEGA laser facility. Wilson et al. applied a technique, extensively used at OMEGA for the last decades,\textsuperscript{6,13,19} to determine the $pR$ of the ablator from the energy downshift of $14.7$-MeV protons produced in surrogate D$^3$He gas-filled CH-capsule implosions; Hicks et al.\textsuperscript{16} implemented an x-ray radiography technique that measures time-resolved $pR$, mass, and velocity of the ablator; and Olson et al.\textsuperscript{17,18} studied x-ray ablation rates in planar geometries for Cu-doped Be, high density carbon, and Ge-doped CH, among other materials. All these techniques have distinctly different but complementary strengths.

This paper is structured as follows: Secs. II and III describe the methods for diagnosing the ablator $pR$ in several types of NIF-capsule implosions, while Sec. IV describes the proposed ablator $pR$ measurements at the NIF. Section V discusses KO-P measurements performed at OMEGA, similar in spirit to those proposed herein for the NIF. Section VI summarizes the main results.

II. DIAGNOSING THE ABLATOR $pR$

13. IN IGNITION-CAPSULE IMPLOSIONS

The current design of the 285 eV indirect-drive ignition capsule consists of a cryogenic deuterium-tritium (DT) layer of 75 $\mu$m with the outer surface positioned at a radius of 1000 $\mu$m. The capsule, which is filled with DT gas in equilibrium at 0.3 mg/cm$^2$, has an outer ablator layer with thickness varying from 90 to 170 $\mu$m depending on the ablator composition. At least three ablator designs are under consideration.\textsuperscript{3,4,20-24} The first design is made of beryllium (Be), doped gradually with copper; the second design is made of CH, doped gradually with germanium; the third design is sign, which is not discussed in this paper, is made of high-density carbon.

Diagnosing the Be-ablator design can be done by utilizing the $\sim 1\%$ residual H (by atom) in the DT fuel, and measuring the energy spectrum of the KO-Ps produced in the fuel. As the KO-Ps produced in the fuel at the fuel-Be-ablator interface lose the least amount of energy, the high-energy endpoint of the KO-P spectrum provides accurate information about the $pR$ of the remaining Be ablator. To quantitatively study how the Be ablator affects the KO-P spectrum, a Monte Carlo code\textsuperscript{8} was used to simulate burn-averaged KO-P spectra for two capsule implosions that are similar to the failed one described in Ref. 25. The density and temperature profiles of the fuel and Be ablator used in the simulations are illustrated in Fig. 1(a). As shown by Fig. 1(a), the density and temperature profiles for the fuel were kept the same, while the density profile for the Be ablator was changed artificially to illustrate the effect of a varying $pR$ on the KO-P high-energy end point. In the simulations, the ablator profile extends out to a radius of 150 $\mu$m (top figure) and to a radius of 220 $\mu$m (bottom figure) corresponding to an ablator $pR$ of 105 mg/cm$^2$ and 210 mg/cm$^2$, respectively. DT fuel with $\sim 1\%$ of residual hydrogen (by atom) was used in the simulations. A primary neutron yield of $5.3 \times 10^{15}$ was computed for both implosions. (b) Simulated KO-P spectra for the two failed implosions. A high-energy endpoint at 10 MeV (top figure) and 6 MeV (bottom figure) was simulated for the implosion with an ablator $pR$ of 105 mg/cm$^2$ and 210 mg/cm$^2$, respectively. Only a small fraction of the produced KO-Ps exit the Be ablator; $\sim 8 \times 10^{10}$ KO-Ps exit the 105 mg/cm$^2$ ablator, and $\sim 3 \times 10^9$ KO-Ps exit the 210 mg/cm$^2$ ablator. These KO-Ps are born in the $\sim 30 \mu$m and $\sim 10 \mu$m outermost regions of the fuel for the 105 mg/cm$^2$ and 210 mg/cm$^2$ ablator cases, respectively. In addition, a decreasing KO-P yield is observed at lower energies when the energy of the emitted KO-Ps is decreasing. This is caused by an increasing fraction of ranged out KO-Ps as the birth energy of these protons decreases. The KO-Ps are fully ranged out at a Be ablator $pR$ of $\sim 260$ mg/cm$^2$.

![FIG. 1. Simulations of two Be-capsule implosions that fail to ignite. (a) The same density and temperature profiles were used for the fuel, while different density profiles were used for the Be ablator, i.e., the ablator extended out to a radius of 150 $\mu$m (top figure) and 220 $\mu$m (bottom figure) corresponding to an ablator $pR$ of 105 mg/cm$^2$ and 210 mg/cm$^2$, respectively. DT fuel with $\sim 1\%$ of residual hydrogen (by atom) was used in the simulations. A primary neutron yield of $5.3 \times 10^{15}$ was computed for both implosions. (b) Simulated KO-P spectra for the two failed implosions. A high-energy endpoint at 10 MeV (top figure) and 6 MeV (bottom figure) was simulated for the implosion with an ablator $pR$ of 105 mg/cm$^2$ and 210 mg/cm$^2$, respectively. Only a small fraction of the produced KO-Ps exit the Be ablator; $\sim 8 \times 10^{10}$ KO-Ps exit the 105 mg/cm$^2$ ablator, and $\sim 3 \times 10^9$ KO-Ps exit the 210 mg/cm$^2$ ablator. These KO-Ps are born in the $\sim 30 \mu$m and $\sim 10 \mu$m outermost regions of the fuel for the 105 mg/cm$^2$ and 210 mg/cm$^2$ ablator cases, respectively. In addition, a decreasing KO-P yield is observed at lower energies when the energy of the emitted KO-Ps is decreasing. This is caused by an increasing fraction of ranged out KO-Ps as the birth energy of these protons decreases. The KO-Ps are fully ranged out at a Be ablator $pR$ of $\sim 260$ mg/cm$^2$.](image-url)
Electron temperature \( (T_e) \) variations typically predicted in the ablator do not significantly affect the \( \rho R \) inferred from the energy downshift of the KO-Ps. To change the inferred ablator \( \rho R \) value by only 1%, one has to change \( T_e \) in the analysis from \( \sim 100 \) eV to an unreasonable value of \( \sim 1000 \) eV. Measuring the high-energy end point of the KO-P spectrum is therefore a sensitive and weakly model dependent method for determining the \( \rho R \) of the remaining Be ablator.

As shown in Fig. 1(b), a much larger fraction of the produced KO-P exit the 105 mg/cm\(^2\) ablator than the 210 mg/cm\(^2\) ablator; \( \sim 8 \times 10^{10} \) KO-P exit the 105 mg/cm\(^2\) ablator, while only \( \sim 3 \times 10^9 \) KO-P exit the 210 mg/cm\(^2\) ablator, which corresponds to a KO-P to neutron yield ratio \( Y_{\text{KO-P}}/Y_n \) of \( \sim 1.5 \times 10^{-5} \) and \( \sim 5.7 \times 10^{-7} \), respectively. These KO-P protons are born in the \( \sim 30 \) µm and \( \sim 10 \) µm outermost regions of the fuel for the 105 mg/cm\(^2\) and 210 mg/cm\(^2\) ablator cases, respectively. The exact trend of how the \( Y_{\text{KO-P}}/Y_n \) ratio varies with increasing \( \rho R \) of the Be ablator is illustrated by the filled circles in Fig. 2. In addition, it should be noted that due to the build up of \( ^3\)He in the fuel, these KO-P measurements could in principle be affected by 14.7 MeV D\(^3\He\) protons. However, simulations indicate that the D\(^3\He\) protons are fully ranged out as they are produced in the innermost 40–50 µm in the fuel (due to the strong temperature dependence of the D\(^3\He\) fusion reaction). As a result, the D\(^3\He\) protons do not affect the KO-P measurements.

The CH-ablator design, which contains naturally large amounts of H, can be diagnosed by measuring the absolute spectrum of KO-P produced in the ablator. In particular, the shape of the measured KO-P spectrum provides information about the ablator \( \rho R \). This is illustrated in Fig. 3, which shows simulations of two capsule implosions. The density and temperature profiles used for the fuel and ablator in these two simulations are shown in Fig. 3(a). Once again, the density and temperature profiles for the fuel were kept the same, while the density profile for the ablator was changed artificially to illustrate the effect of a varying \( \rho R \) on the shape of the KO-P spectrum. In the simulations, the ablator extends to a radius of 150 µm (top figure) and 220 µm (bottom figure) corresponding to an ablator \( \rho R \) of 105 mg/cm\(^2\) and 210 mg/cm\(^2\), respectively. The resulting KO-P spectra, shown in Fig. 3(b), indicate that the change of the ablator \( \rho R \) has a significant impact on the shape of the KO-P spectrum. In contrast, the shape of the KO-P spectrum is not affected significantly by ablator-density-profile variations even though the spatial birth profile of the KO-P depends strongly on the density profile. This is a consequence of the fact that the energy-slowing down of the KO-P is very weakly dependent on mass-density-profile variations. As shown in the references, the energy-slowing down depends mainly on \( \rho R \), while density and temperature effects play minor roles. Other effects, such as time evolution of the ablator \( \rho R \) and fuel-shell mix play minor roles as well, as described in more detail in the next two paragraphs.

Time evolution of the ablator \( \rho R \) has a small effect on the shape of the KO-P spectrum, which significantly simplifies the interpretation of the measured KO-P spectrum. This is illustrated by transporting KO-Ps through density and temperature profiles simulated by the 1D hydrocode LILAC\(^{27}\) at different times for a hydroequivalent capsule implosion at OMEGA. It is meaningful to use this implosion to study how the time-evolution of the ablator \( \rho R \) affects the KO-P spectrum for an ignition-scaled NIF-capsule implosion as the
burn duration and percentage variation of the ablator \( \rho R \) during imploding burn are similar for these implosions. The density and temperature profiles used for this purpose are illustrated in Figs. 4(a) and 4(b), which show the density and temperature profiles at bang time (BT), BT−100 ps, and BT+80 ps for an imploding DT-gas filled CH capsule at OMEGA (a total burn duration of \( \sim 180 \) ps was simulated for this particular implosion). The resulting KO-P spectra for the different times are shown in Fig. 4(c). Each simulated KO-P spectrum was determined assuming a steady-state condition for 60 ps. Despite the fact that KO-Ps are produced before and after bang time, the KO-P spectrum produced at bang time dominates and well represents the burn-weighted spectrum; an indication that a time-integrated measurement of the KO-P spectrum will provide accurate information about the ablator \( \rho R \) at bang time.

Fuel-ablator mix also plays a minor role. As the fuel density and temperature is much lower in the mixed region than in the clean region, the radial source profile of the primary neutrons is not affected by mix to a level that the KO-P spectrum is significantly altered. However, the fuel-ablator mix does alter the ablator-density-profile, but this has no impact on the shape of the KO-P spectrum as already discussed.

Although \( Y_{\text{KO-P}} \) is subject to significant spatial-yield variations caused by magnetic fields surrounding an imploding state, an average \( Y_{\text{KO-P}} \) determined from several measurements can be used to infer a spatially averaged \( \rho R \) of the CH ablator as discussed in Refs. 11 and 12. By using a relatively simple model of an implosion, the \( Y_{\text{KO-P}} \), normalized to the neutron yield \( Y_n \), can be related to the ablator \( \rho R \) by

\[
\frac{Y_{\text{KO-P}}}{Y_n} = \frac{\gamma \sigma_p}{(\gamma+12)m_p} \xi(\rho R)\rho R,
\]

where \( \gamma = n_H/n_C \) (\( \gamma = 1.4 \) for CH); \( \sigma_p \) is the total cross section for the \( np \)-elastic scattering process; \( m_p \) is the proton mass; and \( \xi(\rho R) \) is a function describing the fraction of escaping KO-Ps. Typically \( \sim 200 \) mg/cm\(^2\) of the ablator \( \rho R \) remain at bang time for an ignition-capule implosion, which would generate a KO-P yield of \( \sim 10^{-3} \times Y_n \). As \( Y_{\text{KO-P}} \) is directly proportional to \( \rho R \cdot Y_n \) and the ablator \( \rho R \) and \( Y_n \) are strong functions of the laser drive (a 30%–40% variation in the laser drive changes the ablator \( \rho R \) by a factor of \( \sim 2 \) and the \( Y_n \) by at least a factor of 10), measurements of \( Y_{\text{KO-P}} \) should allow studies of the ablator \( \rho R \) and the drive-physics.

To understand quantitatively how the \( Y_{\text{KO-P}}/Y_n \) ratio varies with \( \rho R \), the remaining CH ablator, several simulations of a capsule implosion were performed. In the simulations, the same density and temperature profiles of the fuel were used as for the capsule implosions shown in Fig. 3(a), while the profile of the CH ablator was changed artificially. The resulting data from these simulations, which are shown in Fig. 5, indicate that the \( Y_{\text{KO-P}}/Y_n \) ratio saturates at \( \sim 10^{-3} \) for \( \rho R \)'s above 150 mg/cm\(^2\). In addition, the escaping fraction reduces from 50% to 10% (relative to the number of produced KO-Ps) as the \( \rho R \) increases from practically zero to

![FIG. 4. (Color) (a) Simulated LL/LAC density profiles at three different times, i.e., at bang time (BT), BT−100 ps, and BT+80 ps for OMEGA shot 39894 (an imploding 3-atm DT filled 27 \( \mu \)m thick CH capsule, which is discussed in more detail in Sec. V). A total burn duration of \( \sim 180 \) ps (FWHM) was simulated for this particular shot when using a flux limiter of 0.06. (b) Corresponding simulated temperature profiles. (c) Simulated KO-P spectra for the three different times (each simulated spectrum was computed assuming a steady-state condition for 60 ps). Also shown in (c) is the total, burn-weighted KO-P spectrum that is very similar in shape to the spectrum produced at bang time, indicating that the time evolution of the ablator \( \rho R \) plays a minor role in the \( \rho R \) analysis of the measured KO-P spectrum.](image)
FIG. 5. Simulated $Y_{KO-P}/Y_n$ ratio (●) and KO-P escaping fraction (○), $\xi$, as a function of $\mu R$ of the CH ablator. The density and temperature profiles of the fuel were kept constant [see Fig. 3(a)] in these simulations, while the density profile and thus $\mu R$ of the ablator was changed. As shown, the yield ratio saturates at $\sim 150$ mg/cm$^2$ and the escaping fraction $\xi$ decreases from $\sim 50\%$ to $\sim 10\%$ as the ablator $\mu R$ increases from zero to $\sim 250$ mg/cm$^2$.

$\sim 250$ mg/cm$^2$. Very relevant to this discussion is that these measurements are not affected significantly by the KO-Ps produced in the fuel (due to the $\sim 1\%$ residual H) as the yield of the escaping KO-Ps, produced in the fuel, is typically orders of magnitude lower than the yield of the escaping KO-Ps produced in the CH ablator (this is understood qualitatively when comparing the data in Figs. 2 and 5). Even at very low ablator $\mu R$, the number of escaping KO-Ps coming from the CH ablator dominates the number of escaping KO-Ps coming from the CH ablator due to the difference in density profile and thus $\mu R$.

FIG. 6. (Color) Simulated KO-P spectra normalized by $Y_n$ for a Cu-doped Be ablator and DT fuel doped with 22% and 25% H (red and black lines). For comparison, the normalized KO-P spectrum for the failed ignition-capule implosion is also shown (blue line). To maintain hydrodynamic equivalence to the ignition-capule implosion, the fuel composition of the H-filled Be-capule implosions are 22% H: 8% D: 70% T and 25% H: 0.5% D: 75% T. The same density and temperature profiles were used in all these simulations [see Fig. 1(a), top graph]. Primary neutron yields of $1.2 \times 10^{13}$ and $7.9 \times 10^{13}$ were simulated for the 22%-H-filled and 25%-H-filled Be-capule implosions, respectively. Although these primary neutron yields are $\sim 4.5$ times and $\sim 6.6$ times lower than for the failed ignition-capule implosion, $Y_{KO-P}$ is in fact $\sim 5$ times higher ($4.5 \times 10^{13}$) and only $\sim 2.5$ times lower ($3.3 \times 10^{13}$) for the 22%-H-filled and 25%-H-filled Be-capule implosions, respectively. As a result, the signal-to-background ($S/B$) ratios are improved significantly as discussed in Secs. III and IV. The same high-energy endpoint of 10 MeV was simulated in all three cases, which involved a 105 mg/cm$^2$ Be ablator.

III. DIAGNOSING THE ABLATOR $\mu R$

IN IMPLoding CAPSULES FILLED WITH HYDROGEN-DEUTERIUM-TRITIUM (HDT) FUEL

Prior to the first ignition experiments, capsules with a Cu-doped Be ablator (or Ge-doped CH ablator), more deuterium-lean fuel mixtures and H-dopant levels up to 25% (by atom) in the fuel will be imploded to primarily reduce the primary neutron yield. To keep these implosions hydrodynamically equivalent to an ignition-capule implosion, and to maintain the cryogenic tritium fuel layering capabilities, stringent requirements on the fuel composition are applied.

Two examples of deuterium-lean fuel compositions that are being considered are 22% H: 8% D: 70% T and 25% H: 0.5% D: 75% T. With a significantly higher H content in the fuel than in the ignition-capule implosion, the HDT-filled Be-capule implosions are more suitable to diagnose KO-Ps as $Y_{KO-P}$ increases and $Y_n$ decreases resulting in a significantly higher signal-to-background ($S/B$) ratio. This is also illustrated in Fig. 6, which shows simulated KO-P spectra (normalized by $Y_n$) for the 22%-H-filled and 25%-H-filled Be-capule implosions, and for the failed ignition-capule implosion. Even though the simulated $Y_n$ for the 22%-H-filled and 25%-H-filled Be-capule implosions is $\sim 4.5$ and $\sim 6.6$ lower, respectively, than for the failed ignition-capule implosion, the KO-P yield is in fact $\sim 5$ times higher and only $\sim 2.5$ times lower, respectively. As a result, the $S/B$ ratio is 22 and 25 times higher for the 22%-H-filled and 25%-H-filled Be-capule implosions, respectively. Further discussions about the absolute $S/B$ ratios can be found in the next section. In addition, as the Be-ablator profile is identical for these capsule implosions, the same high-energy endpoint of 10 MeV was simulated.

IV. PROPOSED ABLATOR $\mu R$ MEASUREMENTS AT THE NIF

The plan is to field several compact CR-39 based proton spectrometers (the spectrometer housing is less than 5 cm in diameter) at various locations around an implosion to diagnose $\mu R$ and $\mu R$ modulations of the remaining ablator at bang time. As the CR-39 efficiency for detecting KO-Ps and background neutrons is 100% and $\sim 6 \times 10^{-3}$, respectively, the...
This absolute yield range combined with the simulated re-
counts are required for inferring an ablator
of KO-P yields ranging from
failed ignition-capsule implosion with ~1% residual H (solid lines) and for the 25%-H-
filled Be-capsule implosion (dashed lines). (b) Absolute $Y_{\text{KO-P}}$ as a function
of $Y_n$ and $\rho R$ for the CH-capsule implosion. In contrast to the Be-ablator
data, $Y_{\text{KO-P}}$ increases with increasing $\rho R$. The white areas in both graphs
indicate the measurable $Y_{\text{KO-P}}$ and $Y_n$ ranges at the NIF. The upper $Y_n$ limit
of $\sim 6 \times 10^{15}$ is determined by detector saturation caused by the neutron
background. In both figures, the lower and upper limits of the measurable
$\rho R$’s are also indicated.

![Graphs showing $Y_{\text{KO-P}}$ and $Y_n$ as functions of $\rho R$ and $Y_n$ for different ablator materials.](image)

**FIG. 7.** (a) Absolute $Y_{\text{KO-P}}$ as a function of $Y_n$ and $\rho R$ for the failed ignition-
capsule implosion with ~1% residual H (solid lines) and for the 25%-H-
filled Be-capsule implosion (dashed lines). (b) Absolute $Y_{\text{KO-P}}$ as a function
of $Y_n$ and $\rho R$ for the CH-capsule implosion. In contrast to the Be-ablator
data, $Y_{\text{KO-P}}$ increases with increasing $\rho R$. The white areas in both graphs
indicate the measurable $Y_{\text{KO-P}}$ and $Y_n$ ranges at the NIF. The upper $Y_n$ limit
of $\sim 6 \times 10^{15}$ is determined by detector saturation caused by the neutron
background. In both figures, the lower and upper limits of the measurable
$\rho R$’s are also indicated.

**FIG. 8.** (a) Signal-to-background ($S/B$) ratios as functions of $Y_n$ for the
failed ignition-capsule implosion with ~1% residual H (solid lines) and for the 25%-H-
filled Be-capsule implosion (dashed lines). (b) $S/B$ ratios as functions of $Y_n$ for the CH-capsule implosion. The horizontal lines in both figures represent the $S/B$ when a standard-counting technique (SCT) is applied
to the data. As shown by the SCT curves, the $S/B$ ratio is independent
of $Y_n$; a result of the fact that the signal scales with $f(\rho R) - Y_n$, while the
background scales only with $Y_n$. A range of $S/B$ ratios of $\sim 0.01$–10 and
$\sim 0.2$–200 is obtained for the failed ignition-capsule implosion with ~1% residual H and 25%-H-filled Be-capsule implosion, respectively; while a $S/B$ ratio varying from ~1 to ~100 is obtained for the CH-capsule implosion. By applying the coincidence-counting technique (CCT) to the low $S/B$ cases ($S/B \ll 1$), the $S/B$ ratios are improved significantly for $Y_n < 10^{16}$. For neutron yields above $10^{16}$, the CCT is not effective due an increased number of background induced random coincidences.

**Dynamic range of the spectrometer**

Dynamic range of the spectrometer is determined mainly by
330 the allowed range of spectrometer distances to the implosion,
331 signal statistics, and signal saturation. About $\sim 10^3$ signal
332 counts are required for inferring an ablator $\rho R$ from either
333 the high-energy end point or the shape of the KO-P spec-
334 trum, and $\sim 10^5$ signal counts per cm$^2$ are required for the
335 CR-39 to saturate. With an active spectrometer area of
336 2 cm$^2$, a range of allowed spectrometer distances of
337 40–550 cm to the implosion and $1/R^2$-scaling of the de-
338 tected KO-P signal, absolute spectra can be measured accu-
339 rately for KO-P yields ranging from $\sim 1 \times 10^7$ to $\sim 4 \times 10^{11}$.
340 This absolute yield range combined with the simulated re-
341 sults shown in Figs. 2 and 5, which illustrate the $Y_{\text{KO-P}}/Y_n$
342 ratio as a function of the ablator $\rho R$, is used to establish the
343 absolute KO-P yield as a function of $Y_n$ and $\rho R$ for the dif-
344 ferent ablators (see Fig. 7). The Be-ablator curves, shown in
345 Fig. 7(a), indicate a tolerable $Y_n$ ranging from $\sim 5 \times 10^9$ to
346 $\sim 10^{16}$ [the solid and dashed line is for the failed ignition-
347 capsule implosion (with ~1% residual H) and 25%-H-filled
348 Be-capsule implosion, respectively]. However, as the $\rho R$ of
349 the Be ablator approaches 240 mg/cm$^2$, $Y_{\text{KO-P}}$ decreases sig-
350 nificantly to the point where the $S/B$ ratio is well below 1. At
351 this point, the CR-39 saturation is dictated by the neutron
352 background. Based on the information in Ref. 29, an upper
353 $Y_n$ limit of $\sim 6 \times 10^{15}$ is determined for a spectrometer posi-
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Fig. 8. Carlo simulations of differences in the spectral shape are well modeled by steady-state Monte Carlo simulations, e.g., varying from 20 to 50 mg/cm$^2$. A quick assessment of the $\rho R$ value in a certain direction can be done by looking at what energy the KO-P spectrum flattens out; for the 20 mg/cm$^2$ and 50 mg/cm$^2$ the spectrum flattens out at $\sim$12.5 MeV and $\sim$10 MeV, respectively.

\begin{center}
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\textbf{FIG. 9.} (Color) A subset of KO-P spectra measured simultaneously in four different directions for OMEGA implosion 39894 (3 atm of DT fuel in a 27 $\mu$m thick CH shell, illuminated by 60 laser beams delivering 23 kJ of laser energy in a 1-ns square pulse). Narrow-band-width spectrometers that only cover the high-energy portion of the spectrum were used in these measurements. Each spectrum was normalized to the average KO-P yield of $1.5 \times 10^{10}$. With a measured neutron yield of $6.5 \times 10^{10}$, the average $S/B$ ratio is $\sim$10 when using the standard counting technique (SCT). The observed differences in the spectral shape are well modeled by steady-state Monte Carlo simulations (red spectra), which indicate significant low-mode $\rho R$ modulations, e.g., varying from 20 to 50 mg/cm$^2$. A quick assessment of the $\rho R$ value in a certain direction can be done by looking at what energy the KO-P spectrum flattens out; for the 20 mg/cm$^2$ and 50 mg/cm$^2$, the spectrum flattens out at $\sim$12.5 MeV and $\sim$10 MeV, respectively.

\begin{figure}[h]
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\includegraphics[width=\textwidth]{fig9.png}
\caption{(Color) A subset of KO-P spectra measured simultaneously in four different directions for OMEGA implosion 39894 (3 atm of DT fuel in a 27 $\mu$m thick CH shell, illuminated by 60 laser beams delivering 23 kJ of laser energy in a 1-ns square pulse). Narrow-band-width spectrometers that only cover the high-energy portion of the spectrum were used in these measurements. Each spectrum was normalized to the average KO-P yield of $1.5 \times 10^{10}$. With a measured neutron yield of $6.5 \times 10^{10}$, the average $S/B$ ratio is $\sim$10 when using the standard counting technique (SCT). The observed differences in the spectral shape are well modeled by steady-state Monte Carlo simulations (red spectra), which indicate significant low-mode $\rho R$ modulations, e.g., varying from 20 to 50 mg/cm$^2$. A quick assessment of the $\rho R$ value in a certain direction can be done by looking at what energy the KO-P spectrum flattens out; for the 20 mg/cm$^2$ and 50 mg/cm$^2$, the spectrum flattens out at $\sim$12.5 MeV and $\sim$10 MeV, respectively.}
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\textbf{FIG. 10.} (Color) Modeling of a capsule implosion, using a simple ice-block-implosion model, to illustrate the relationship between $\rho R$ and the shape of the KO-P spectrum. (a) The ice-block-implosion model. A constant shell density of 20 g/cm$^3$ was used in the model, while the shell thickness was increased in steps of 10 $\mu$m (a fixed $T_e$ of 500 eV was used as well). A neutron point source at the center of the implosion was also used in these simulations. (b) Simulated KO-P spectra for four different $\rho R$'s ranging from 20 to 80 mg/cm$^2$. The spectral shapes indicate a strong correlation between the $\rho R$ and the energy at which the KO-P spectrum flattens out. Looking at specifically the KO-P spectrum for the 80 mg/cm$^2$ case, it is clear that this correlation is a result of the fact that the maximum energy of the escaping KO-Ps produced at, say, 20, 30, 40, and 50 mg/cm$^2$ cannot be higher than 9.3, 10.2, 12.5, and 14 MeV, respectively.

\begin{figure}[h]
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\includegraphics[width=\textwidth]{fig10.png}
\caption{(Color) Modeling of a capsule implosion, using a simple ice-block-implosion model, to illustrate the relationship between $\rho R$ and the shape of the KO-P spectrum. (a) The ice-block-implosion model. A constant shell density of 20 g/cm$^3$ was used in the model, while the shell thickness was increased in steps of 10 $\mu$m (a fixed $T_e$ of 500 eV was used as well). A neutron point source at the center of the implosion was also used in these simulations. (b) Simulated KO-P spectra for four different $\rho R$'s ranging from 20 to 80 mg/cm$^2$. The spectral shapes indicate a strong correlation between the $\rho R$ and the energy at which the KO-P spectrum flattens out. Looking at specifically the KO-P spectrum for the 80 mg/cm$^2$ case, it is clear that this correlation is a result of the fact that the maximum energy of the escaping KO-Ps produced at, say, 20, 30, 40, and 50 mg/cm$^2$ cannot be higher than 9.3, 10.2, 12.5, and 14 MeV, respectively.}
\end{figure}

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V. MEASUREMENTS PERFORMED AT OMEGA

Diagnosing shell $\rho R$ and $\rho R$ modulations of gas-filled CH-capsule implosions have been performed routinely at OMEGA for more than a decade. In many of those experiments, which are similar to the ablator measurements proposed at the NIF, up to nine charged-particle spectrometers were fielded around an implosion. An example of resulting data from those experiments is illustrated in Fig. 9, which shows a subset of four KO-P spectra obtained from a single high-adiabat implosion involving a capsule with a 27 $\mu$m CH shell filled with 3 atm of DT gas (shot 39894).

$\rho R$'s varying from 20 to 50 mg/cm$^2$ were inferred from the Monte Carlo simulated fits (red spectra) to the measured...
Thickening was increased in steps of 10 µm, which the shell density was kept constant, while the shell thickness was increased in steps of 10 µm (a constant electron temperature of 500 eV was used as well). For simplicity a neutron point source at the center of the implosion was used in these simulations. As shown in Fig. 10b, the resulting KO-P spectra indicate a strong correlation between the pR and the energy at which the KO-P spectrum flattens out.

Looking at specifically the KO-P spectrum for the 80 µg/cm² case, it is now clear that this correlation is a result of the maximum energy of the escaping KO-Ps produced at, say, 20, 30, 40, and 50 µm cannot be higher than 9.3, 10.2, 12.5, and 14 MeV, respectively.

VI. SUMMARY

We propose to accurately determine the areal density (pR) of NIF-capsule implosions using charged-particle spectrometry. By fielding several very compact charged-particle spectrometers in different positions around the implosion, pR and pR modulations of the remaining ablator can be obtained through absolute measurements of yield and spectra of knock-on protons (KO-P). The results from several simulations of ignition-capsule and H-filled capsule implosions at the NIF and experiments performed at OMEGA clearly indicate that measurements of KO-P spectrum at various locations around an implosion can provide accurate information about pR and pR modulations of a variety of ablator compositions for neutron yields up to ~6×10¹⁵ and ablator pR up to ~240 mg/cm². In addition, due to the continuous improvements of the spectrometry techniques and CR-39 processing and analysis techniques, it is realistic to assume that the pR of the remaining ablator at bang time can be diagnosed accurately for significantly higher neutron yields than 6×10¹⁵.

S. P. Hatchett explored the idea of using knock-on deuterons (KO-D) to diagnose the beryllium ablator. However, it turned out that this was not feasible as the KO-Ds have a relatively short range.
As CR-39 detectors are used in the proton spectrometers, the signal \( S \) scales with hydrogen content in the fuel times primary neutron yield \( Y_n \) (Ref. 19) while the background \( B \), which is mainly due to neutrons, only scales with \( Y_n \) (Ref. 29). As a result, the \( S/B \) ratio increases with increasing hydrogen content in the fuel.

By correlating the front and back side scans of the CR-39 data, most of the background is rejected, which significantly improves the \( S/B \).

The CCT utilizes the fact that a signal event produces a track on both the front and back side of a thin piece of CR-39, while a neutron-background event produces only a track on either the front or back side of the CR-39.

The CCT utilizes the fact that a signal event produces a track on both the front and back side of a thin piece of CR-39, while a neutron-background event produces only a track on either the front or back side of the CR-39.
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